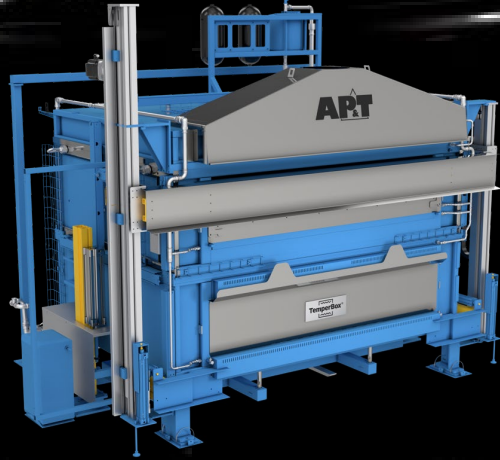




Analysis of process limits for partial hot stamping with controlled pre-cooling by radiation exchange

Alborz Reihani, Leonore Donat, Sebastian Heibel, Thomas Schweiker, Alper Güner, Marcus Gienger, Maik Winderlich, Marion Merklein

Mercedes-Benz



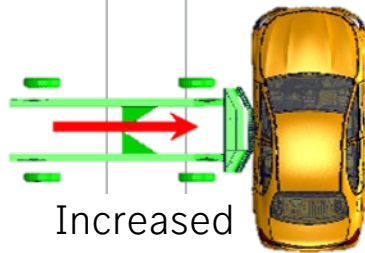
Analysis of process limits for partial hot stamping with controlled pre-cooling by radiation exchange

1. Introduction and motivation
2. Investigation methods and materials
3. Experimental setup and corresponding simulation model
4. Results and discussion
5. Summary and outlook

Introduction and motivation

Higher safety requirements for the car body

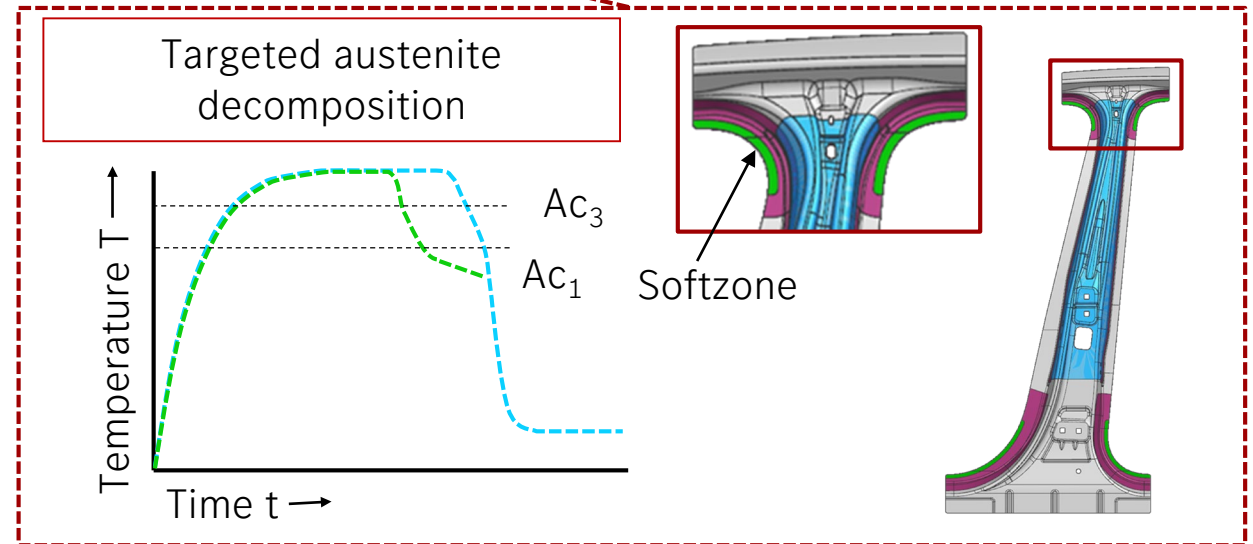
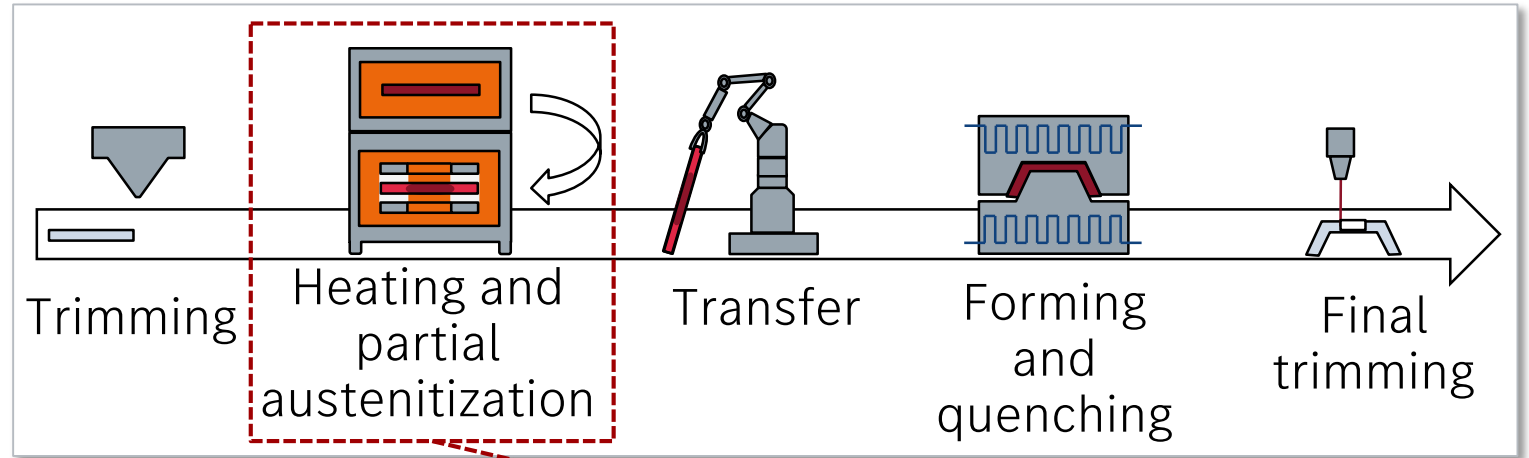
*IIHS old!: 50 km/h;1500 kg



Increased requirements

*IIHS new since 2022: 60 km/h;1900 kg

*Insurance Institute for Highway Safety



Investigation methods and materials

Investigation methods

- Experimental trials
- FE-simulation with AutoForm®R10

Materials

- 22MnB5 AS150
- 8MnB7 AS150
- Blank 8MnB7 and patch 22MnB5

Parameter

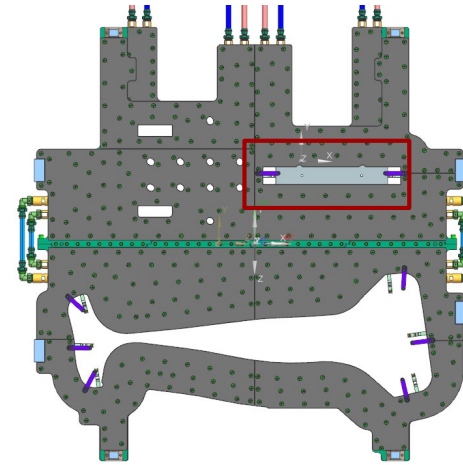
- Sheet thickness t_0
- Partial pre-cooling time $t_{\text{pre-cooling}}$

Objectice

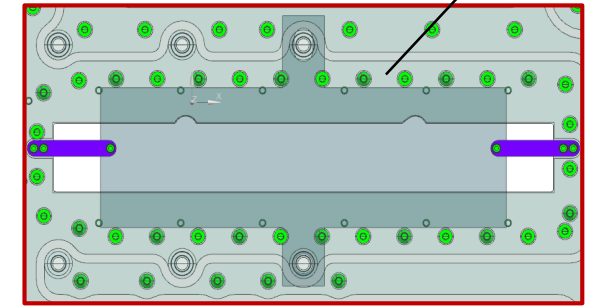
Simulative and experimental analysis of **phase transformation** and **hardness** using different sheet thicknesses and materials

⇒ Elaboration of possible process limits

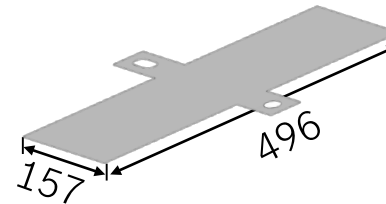
Mask



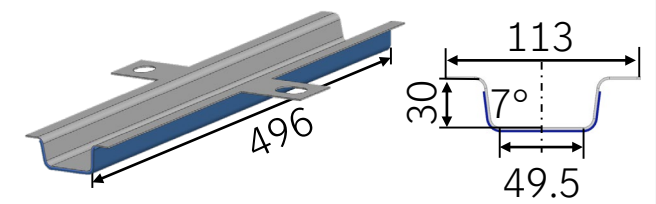
Covered area



Blank



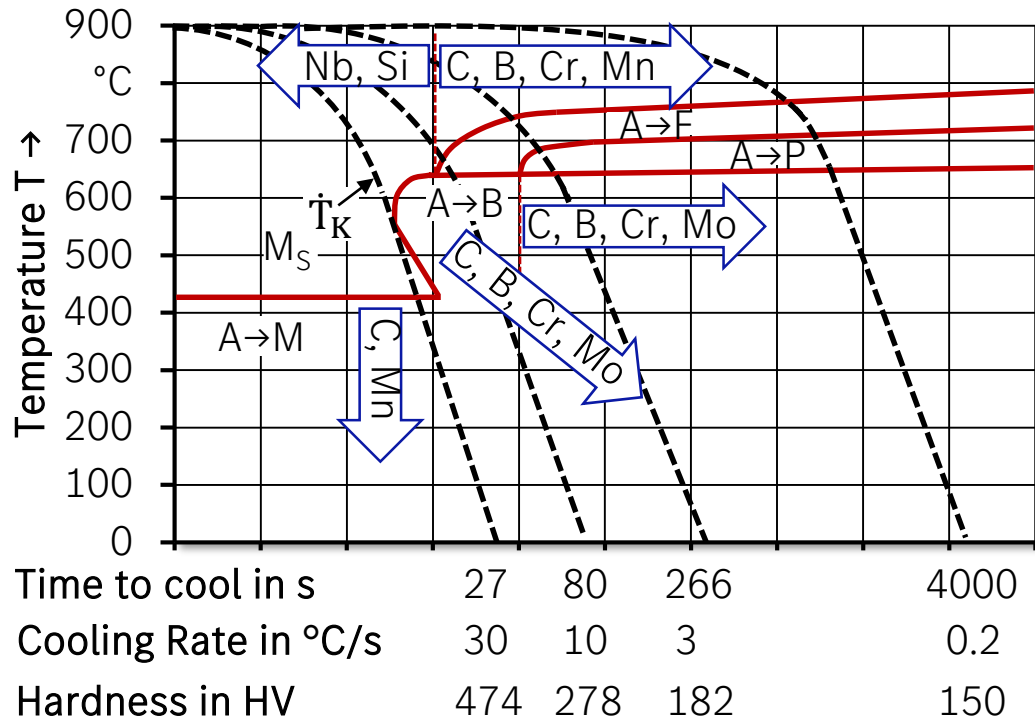
Patched-hat profile



CCT-Diagram of 8MnB7 and 22MnB5

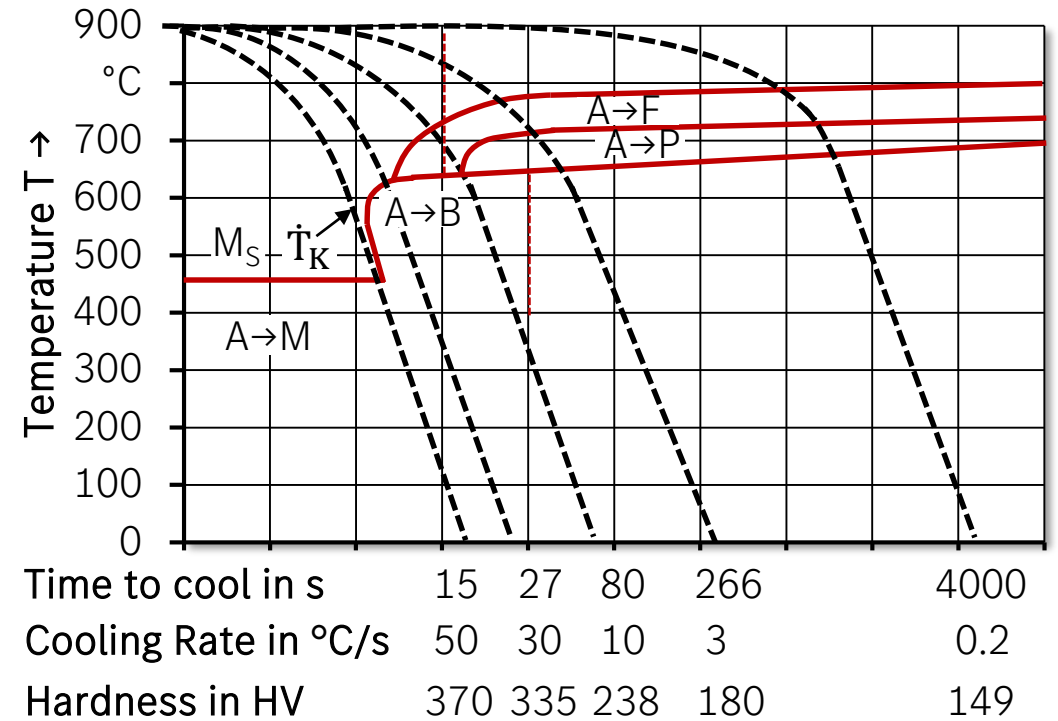
Shifting phase transformation areas due to chemical composition

22MnB5



[1]

8MnB7



[2]

A: Austenite

B: Bainite

F: Ferrite

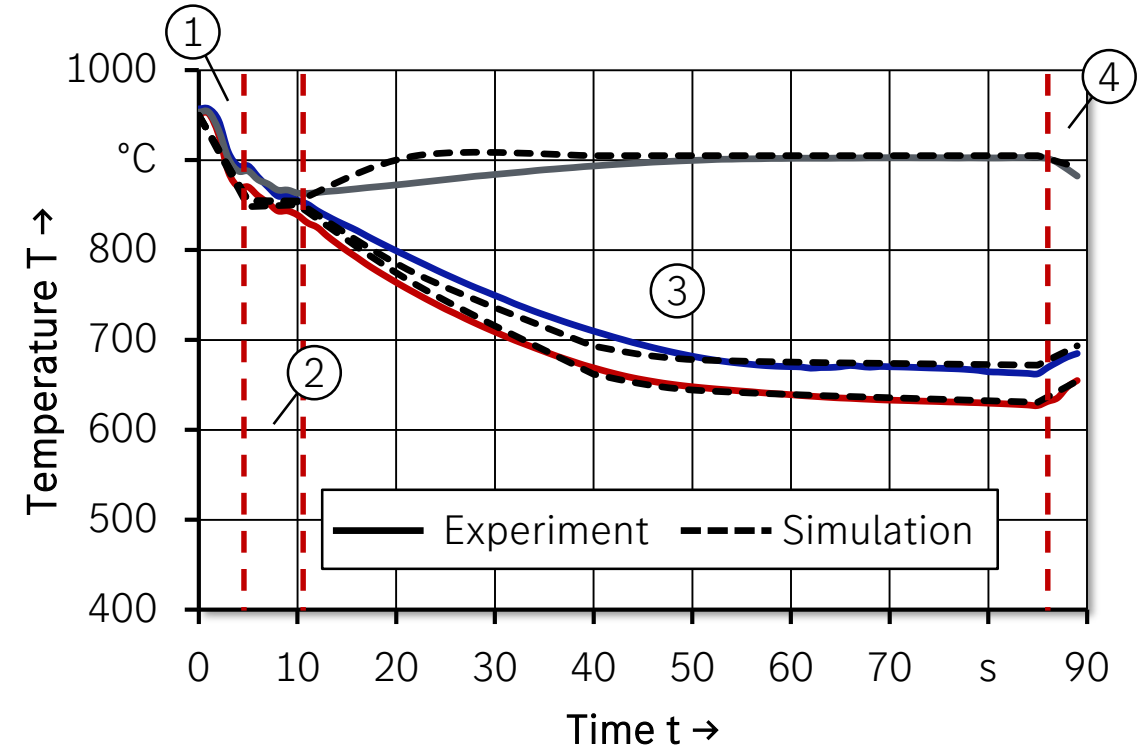
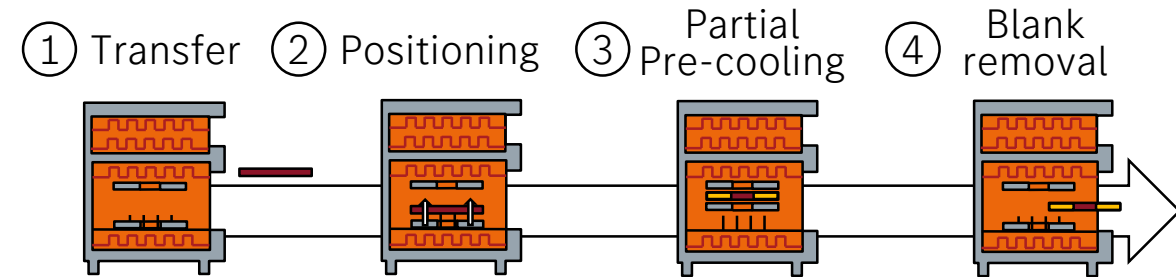
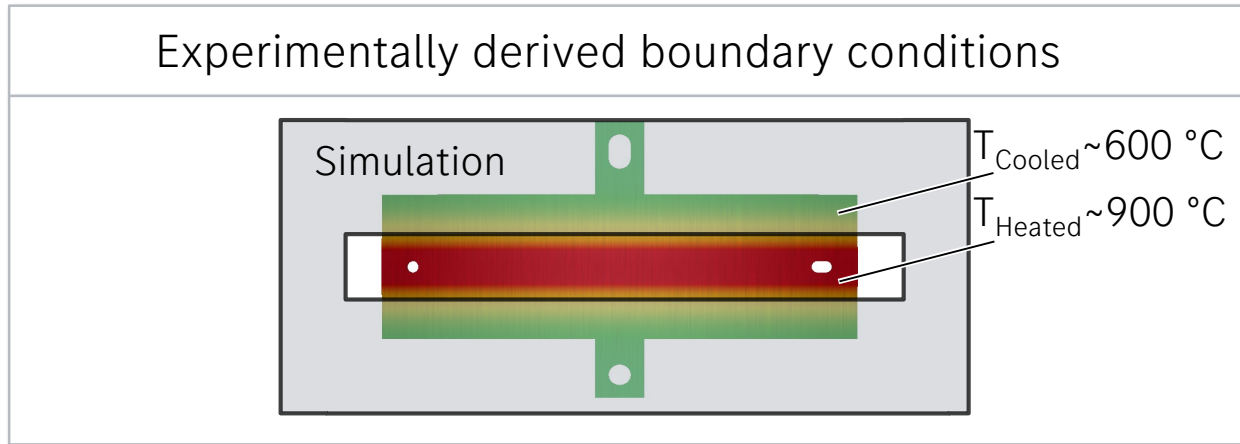
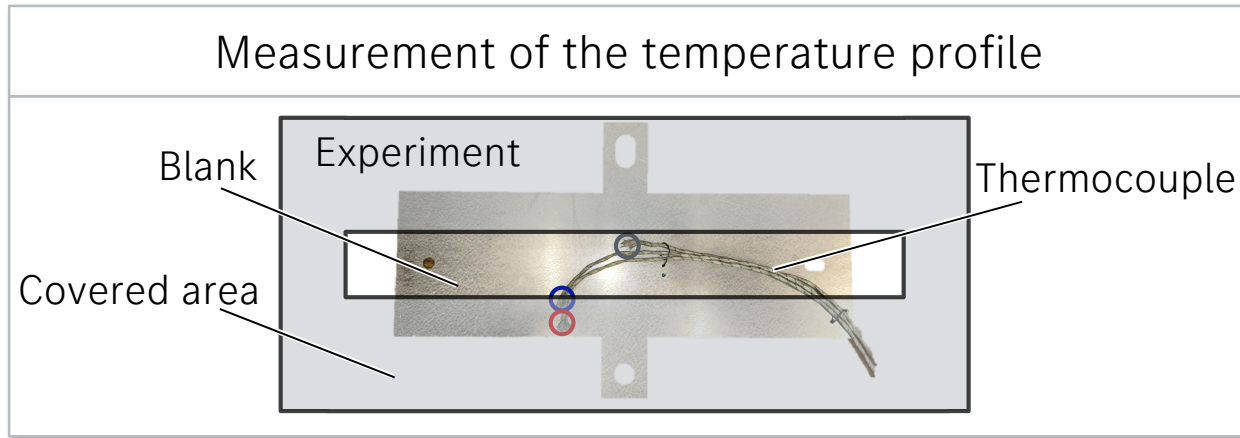
P: Pearlite

M: Martensite

 M_s = Martensite Start Temp.

Temperature measurements and simulation of partial pre-cooling

Temperature-input for the simulation is derived from experimental measurements

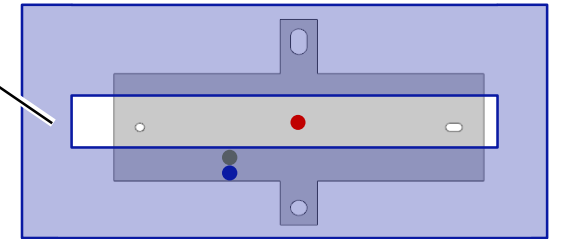


Influence of the sheet thickness

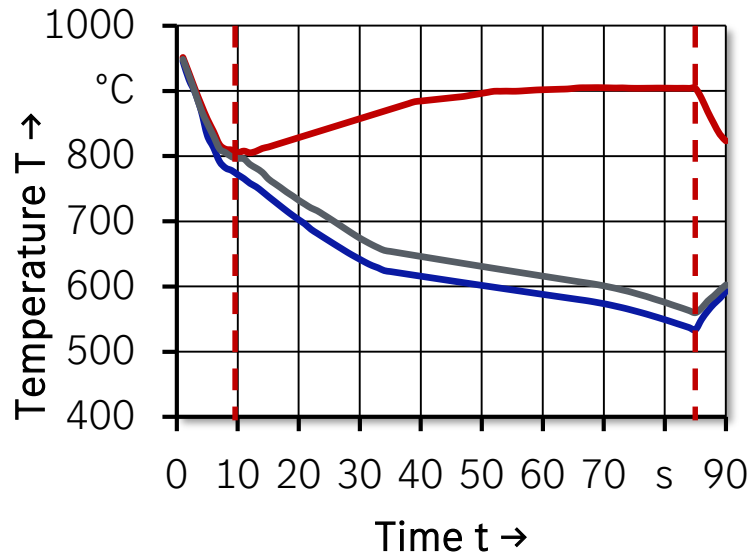
Significant influence on temperature profile, cooling rate and phase transformation

— Heated — Cooled (20 mm from the edge) — Cooled (5 mm from the edge)

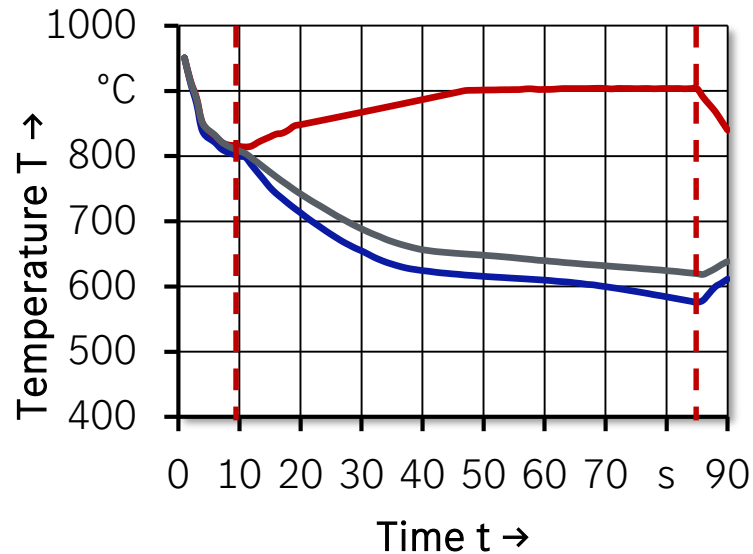
Covered area



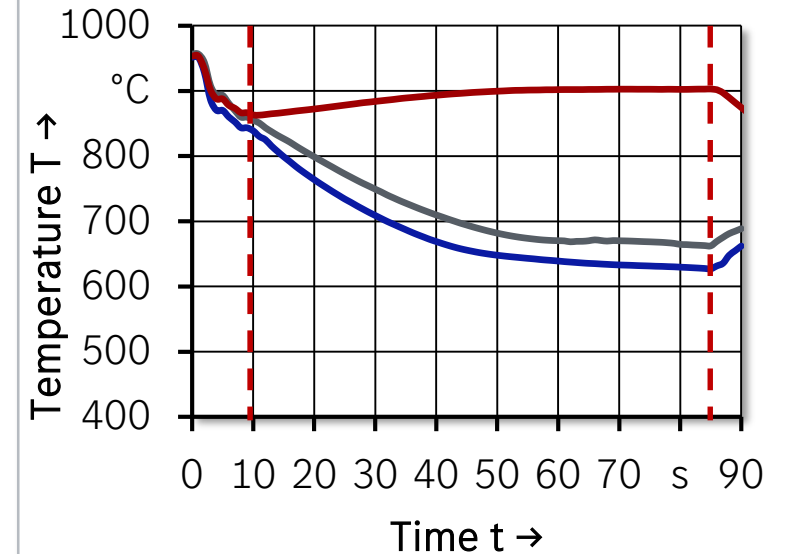
0.80 mm



1.15 mm



1.50 mm

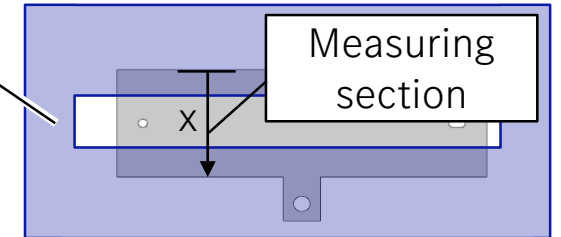


Hardness - 8MnB7 and 22MnB5

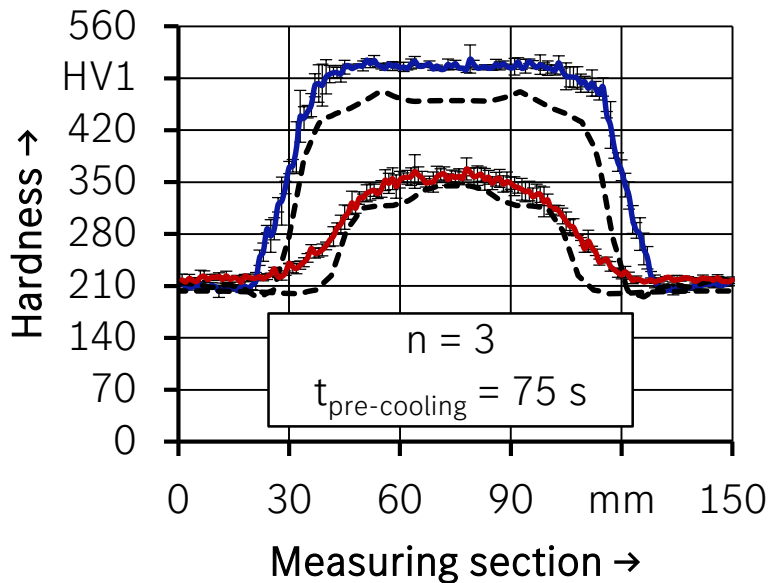
Sheet thickness influences the formation of soft, transition and hard areas

----- Simulation — Experiment (8MnB7) — Experiment (22MnB5)

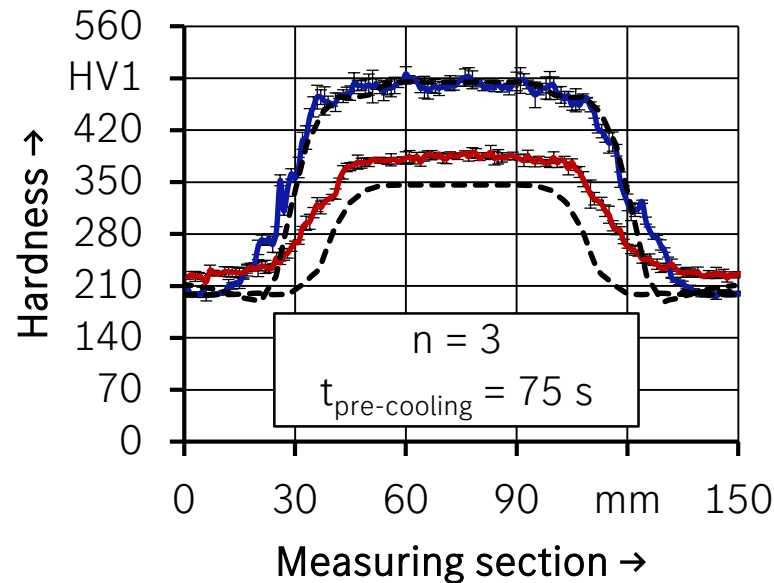
Covered area



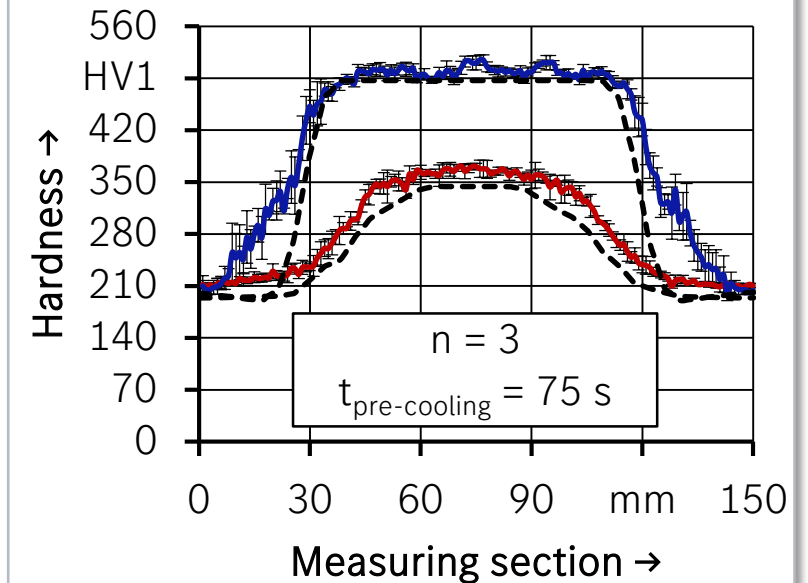
0.80 mm



1.15 mm



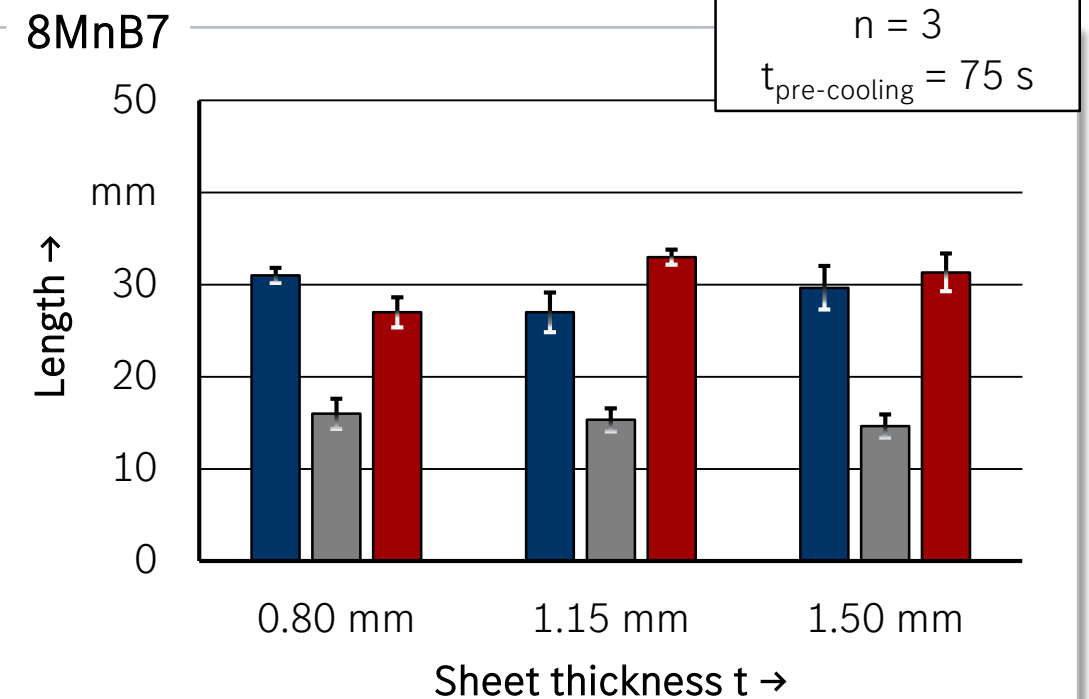
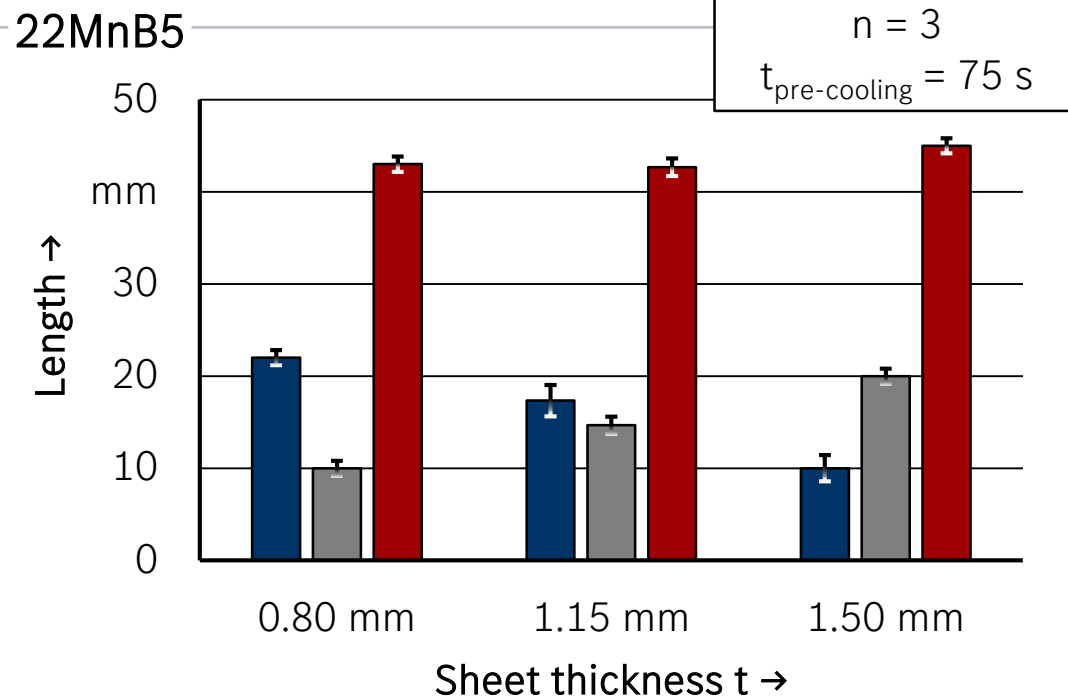
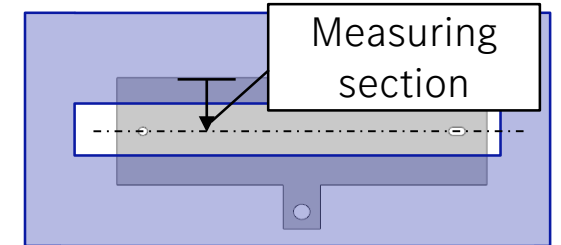
1.50 mm



Hardness - 8MnB7 and 22MnB5

Sheet thickness influences the formation of soft, transition and hard areas

■ Soft zone (< 240 HV) ■ Transition zone ■ Hard zone (> 420 HV 22MnB5)
(> 330 HV 8MnB7)



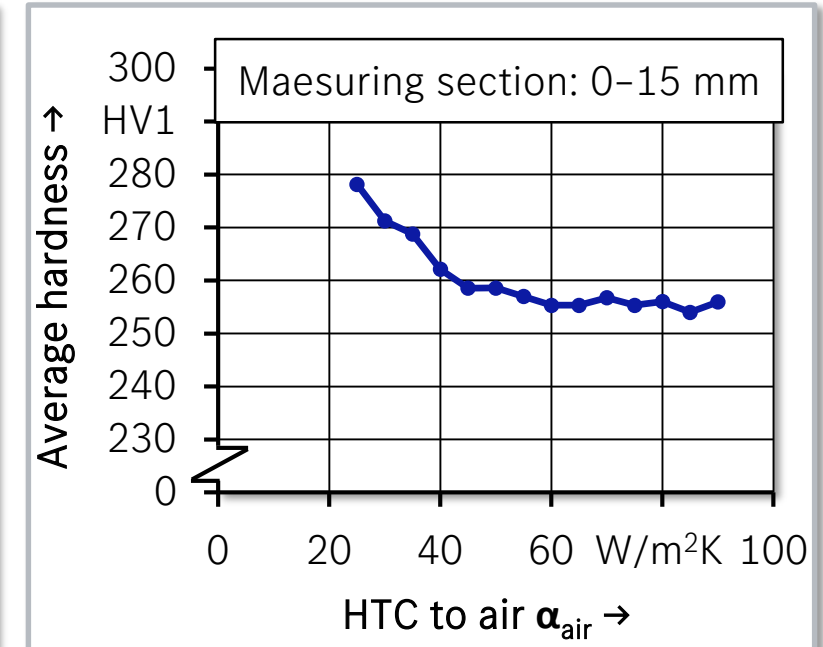
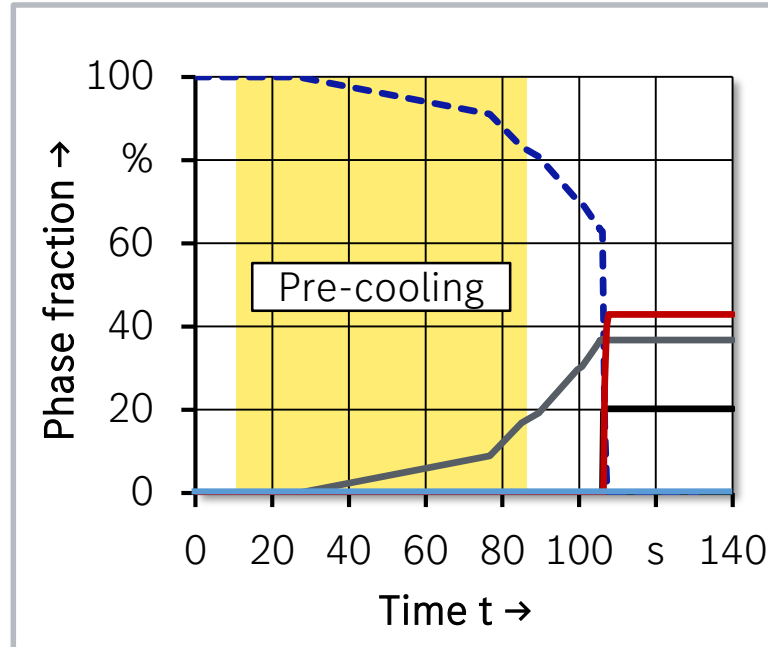
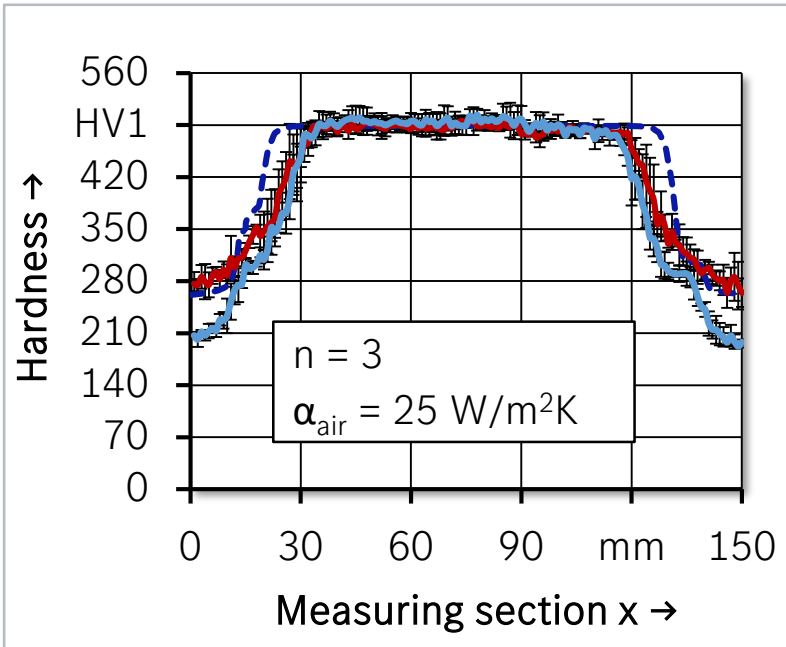
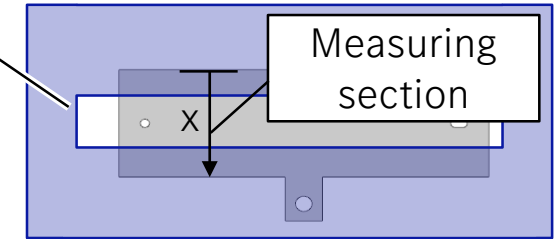
Hardness - Sheet thickness of 2.25 mm - 22MnB5

Extended pre-cooling times are required for the formation of soft areas

— Experiment $t_{\text{pre-cooling}} = 75$ s
 - - - Simulation $t_{\text{pre-cooling}} = 75$ s
 — Experiment $t_{\text{pre-cooling}} = 105$ s

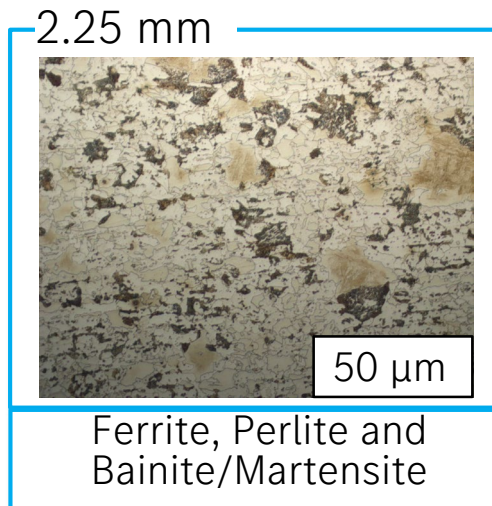
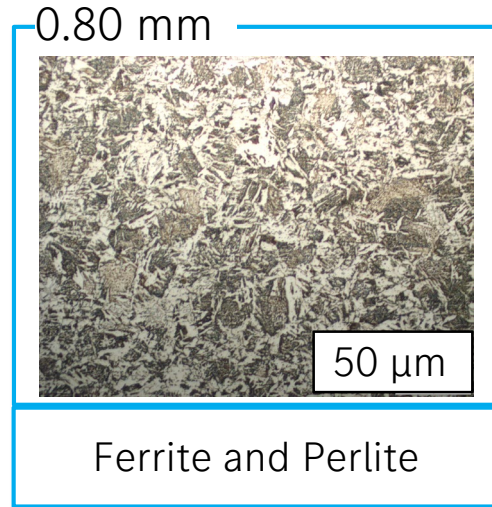
- - - Austenite — Martensite
 — Bainite — Pearlite
 — Ferrite

Covered area

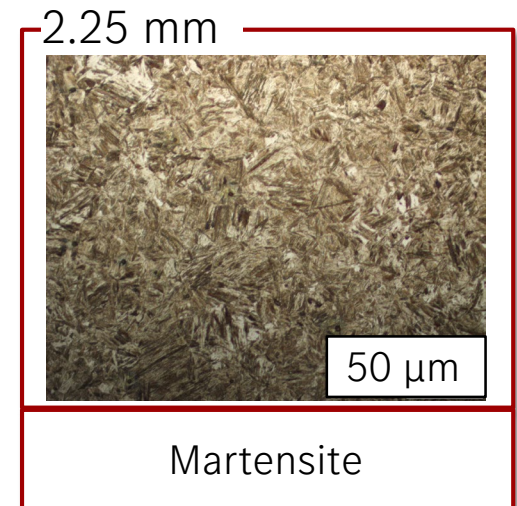
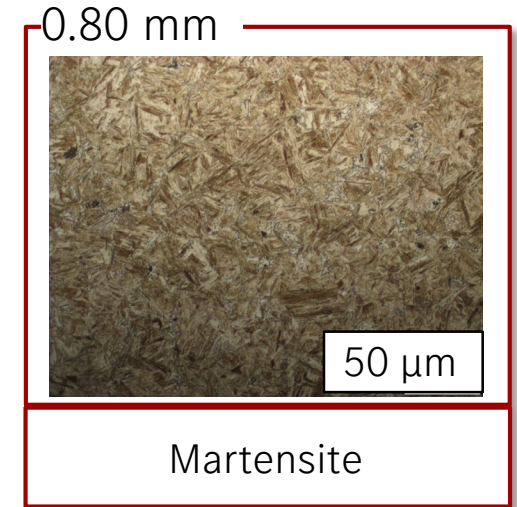
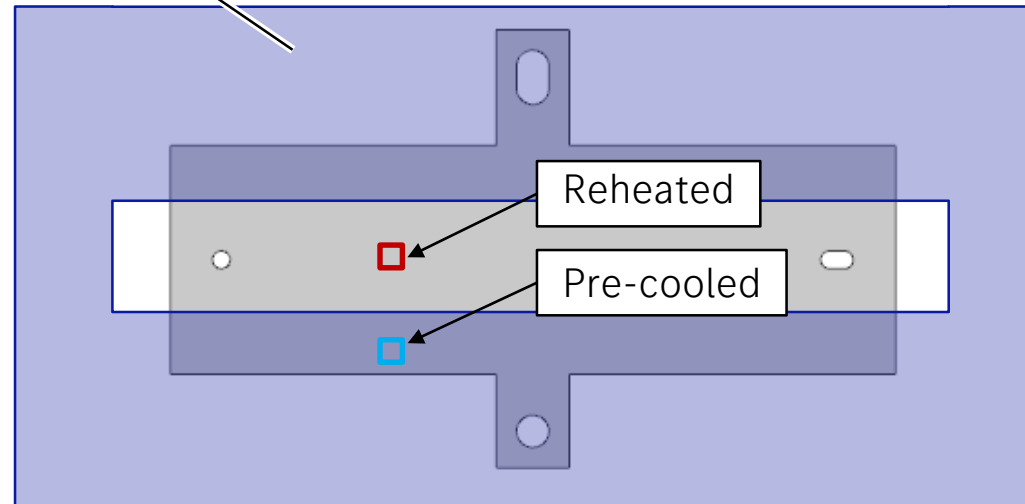


Microstructure analysis - 22MnB5

Higher proportion of hard phases in the overall microstructure at 2.25 mm

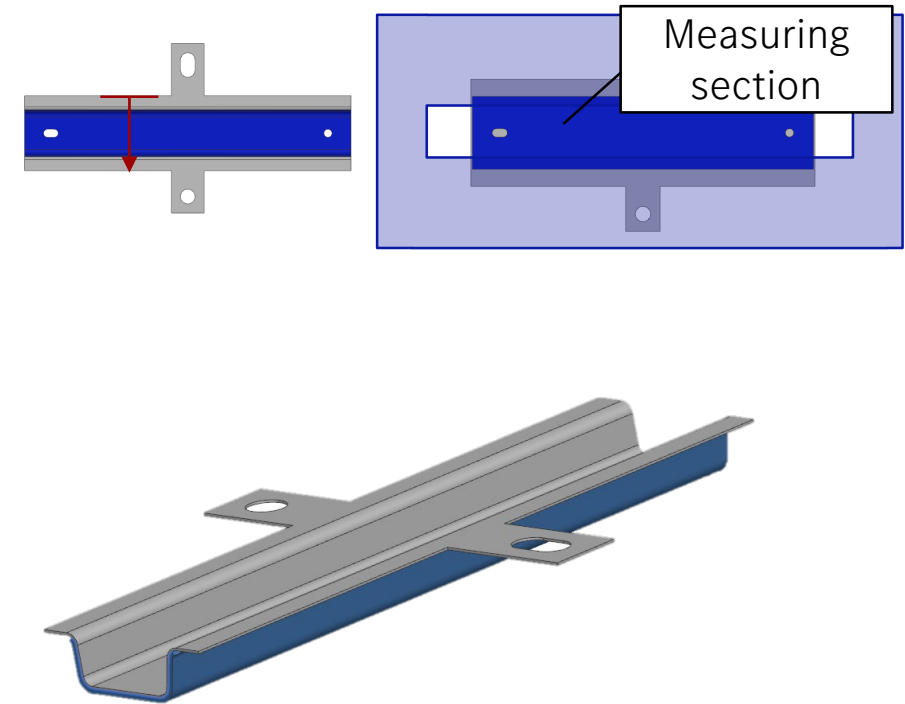
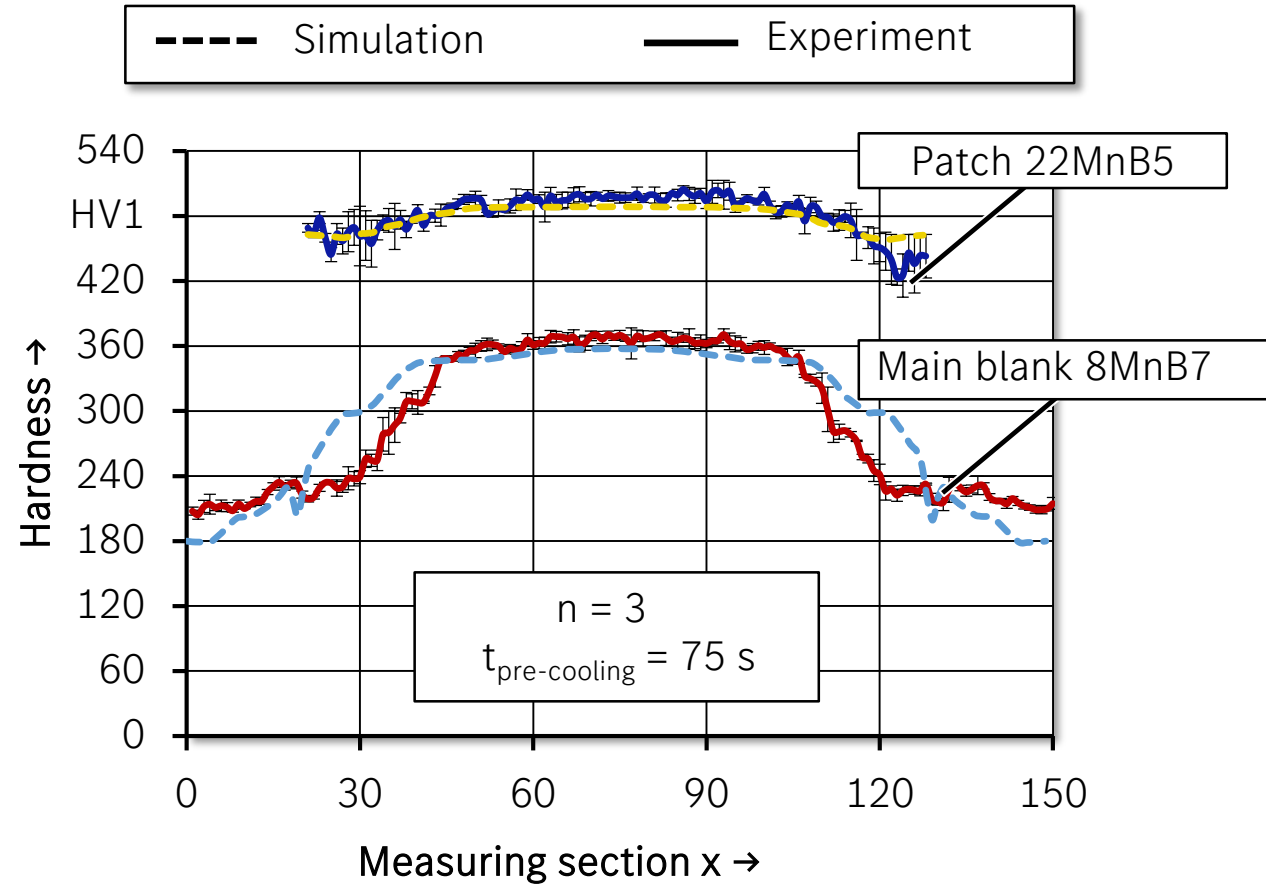


Covered area



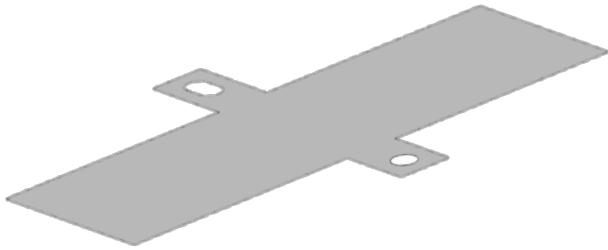
Patched-hat profile

TemperBox® process affects hardness of the patch



Summary

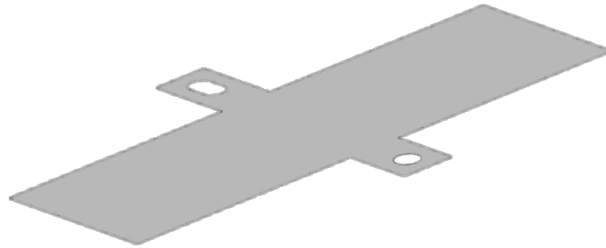
Flat blank



$t_0 = 0.8 \text{ mm}, 1.15 \text{ mm and } 1.50 \text{ mm}$

- The carbon content influences the final hardness profile significantly
- Good correlation of simulation and experiment

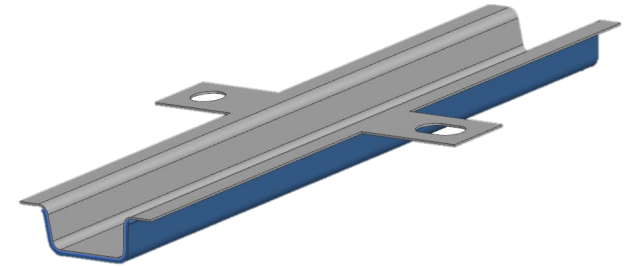
Flat blank



$t_0 = 2.25 \text{ mm}$

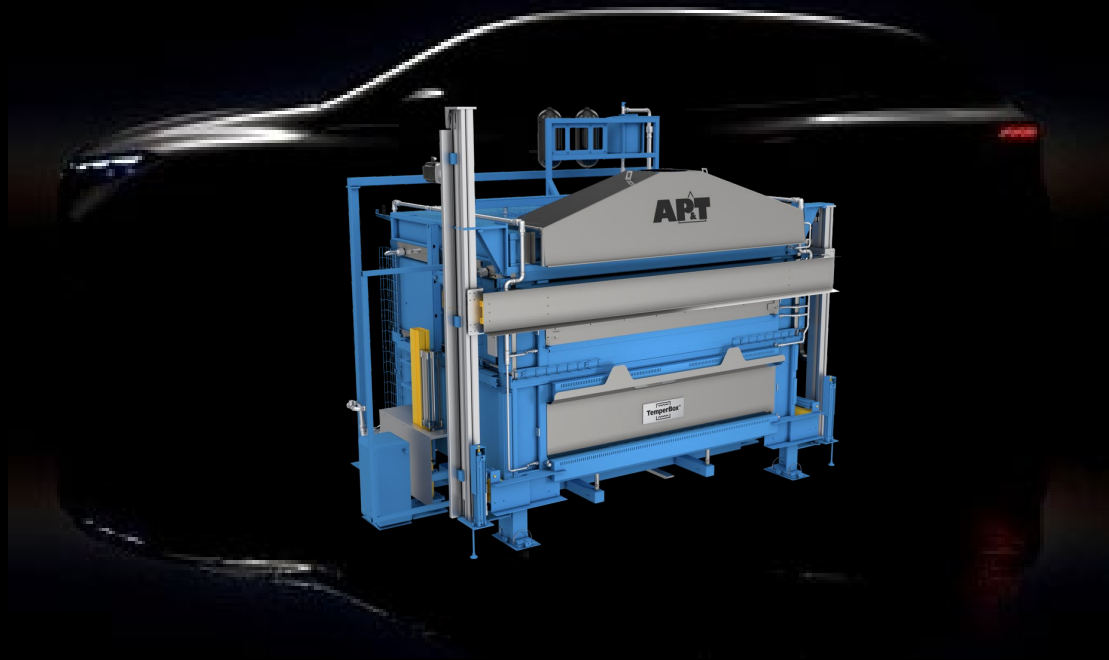
- 75 s pre-cooling time is not sufficient to form homogeneous soft areas
- Simulatively the heat transfer coefficient to air is of importance

Patched-hat profile



$t_{\text{patch}} = 1.25 \text{ mm and } t_{\text{blank}} = 1.50 \text{ mm}$

- Partial pre-cooling slightly affects hardness of the patch
- Deviation between simulation and experiment in the transition area



Thank you
for your attention.

References

- [1] Mohrbacher H 2014 Martensitic Automotive Steel Sheet - Fundamentals and Metallurgical Optimization Strategies *Advanced Materials Research* **1063** 130–42.
- [2] Güner A, Sonntag M, Philippot C, Bittendiebel J, Sarre B, Dormegnny L, Reihani A and Heibel S2022 Experimental and numerical investigation of final product properties of Ductibor® 1000 AS under different process conditions, 8th *Int. Conf. Hot Sheet Metal Forming of High-Performance Steel*, May30th–June 2nd, Barcelona, Spain.